AMENDMENTS TO THE SPECIFICATION

Page 3

Please replace the paragraph at page 3, line 5 with the following amended paragraph:

In one embodiment of the tensioning means in accordance with the invention, in which the upper run of the mast is braced and biased, the tensioning means is guided to the upper portion of the mast by a tensile unit or winch provided on the crane superstructure, via at least one pylon and/or at least one bracing support. The pylon or pylons can be fastened, swivelling, in the area of the crane superstructure and in particular can be arranged protruding obliquely from the level luffing plane, in order to also be able to absorb forces arising obliquely with respect to the level luffing plane.

Please replace the paragraph at page 3, line 15 with the following amended paragraph:

Two tensioning means can be provided for the upper run of the mast, and additionally or alternatively for the lower run of the mast, one on each side respectively (at a distance from the level luffing plane).

Page 4

Please replace the paragraph at page 4, line 1 with the following amended paragraph:

In accordance with another aspect of the present invention, a tensioning system is provided, in which the tensile units or winches on the crane superstructure are at a distance from the level luffing plane of the telescopic mast of the crane, such that the tensioning means can absorb a substantial proportion of the loads having components perpendicular to the level luffing plane. This ensures that lateral loads, for example loads from wind pressure, which act in any direction transverse to the level luffing plane can also be absorbed and compensated for within the

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tensioning system in accordance with the invention. In such designs, it is favourable to arrange the tensioning means tensile units or winches for bracing the upper run of the mast behind the mast joint of the crane superstructure, since they can then simultaneously act as a counterweight.

Page 7

Please replace the paragraph at page 7, line 1 with the following amended paragraph:

The telescopic mast is tensioned towards both sides of the level luffing plane, the components in Figure 1B are only provided with reference numerals on the left-hand side. The tensioning system functions as follows:

Please replace the paragraph at page 7, line 4 with the following amended paragraph:

Starting from the cable winch 3, the tensioning cable 1 runs as its outer portion 1b firstly over a roller 8 on the pylon 9 which is fastened, swiveling swivelling, to the crane superstructure as shown by the arrows. From the roller 8, the cable 1b passes through the gantry 10 and at the roller 4 at the tip of the mast is turned and deflected into the telescopic jib, where it runs as its inner portion 1a along the inner side of the jib to the lower portion of the first telescopic portion 5, where it is secured on the fastening 6. The bias of the cable via the counterweights 2 is explained in more detail by way of Figure 3. As follows from Figure 1B, the winches 3 are situated laterally left and right away from the level luffing plane and so provide the possibility of also supporting lateral forces. The mast 7 and the tensile cable 1 form one unit in all bearing states and while traveling travelling on roads.

Please replace the paragraph at page 7, line 14 with the following amended paragraph:

The telescopic mast is pressure-biased or compressed axially in its upper cross-sectional part on its upper run 7a due to the effect of the force in the cable sections 1a and 1b. The upper run 7a, consisting of high-tensile steel, can directly absorb this pressure bias. If the telescopic mast is then loaded with weight, the resultant tensile forces in the upper cross-section act against the

pressure forces from the bias. The bias or compression and the material is relieved at these points, such that large, undesirable deformations can be avoided. The bending beam is omitted. Figures 2A and 2B show the same views as in Figures 1A and 1B, but with the difference that in this case a design has been chosen which ensures an increased lateral stability of the telescopic mast. To this end, longer, additionally coupled pylons 9a are provided which protrude outwards, i.e. laterally away from the level luffing plane, and upwards. These pylons 9a can be linearly adjustable and they adjust the distance between the tensile cables and the main axes of the jib, so as to make it possible to adapt the direction of the effect of the bracing. A higher transverse stabilization stabilisation is provided, in addition to the longitudinal bracing provided, and the pressure bias acts in the same way as explained with respect to Figures 1A and 1B.

Please replace the paragraph beginning at page 8, line 17 with the following amended paragraph:

It may be generally stated that maximum admissible stresses in the peripheral fibers fibres, both in the jib (telescopic mast) and in the turntable support for the counterweight, caused by bending, are compensated for by the biasing and bracing in accordance with the invention. The material and deformations can be further optimized optimised, if the appropriate bias pressure stresses can also be created converted into a tensile stress in the lower cross sectional part of the jib run. This is achieved, for example, in an embodiment in accordance with Figures 5A and 5B, in which the telescopic mast 7 is biased and braced both above and below the center centre line. The bracing on the upper run in the embodiment in accordance with Figures 5A and 5B corresponds to that of Figures 1A and 1B. Additionally in this case, however, bracing and biasing is also realized realised in the lower cross sectional part of the jib run, namely via the winch 17 fastened to the front of the crane superstructure, from which a tensile cable 11 runs, from which the portion 11b firstly runs to the upper roller 14 where it is turned and deflected and runs as the portion 11a to the fastening 16 on the first extending telescopic portion 5. The material and deformations can be optimized optimised even further, since the pressure stress in the lower run 7b can be converted into a tensile stress using this measure. The tensioned cable sections 11a and 11b on the lower run impose a compressive bias help to bear the load, since

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they are biased. If the telescopic mast 7 is loaded by lifting a load, the pressure stress in the jib is not increased, rather Rather, the tensile stress in the cables 11a, 11b is dissipated as it is replaced by the load acting on the lifting cable. A In this way a lifted load remains substantially at the same point; and deformation of the mast usually resulting from the lifting operation is minimised minimized. Fatigue strength problems are reduced even further due to lower deformation and lower stress differences. The deformation of such a biased system is also then even significantly lower with respect to a non-biased system, if the tensile stress in the cables is fully dissipated and the latter have become slack. Using an upper and lower bias and bracing, damaging stress peaks are avoided, material is saved on, deformation is minimized minimised and the bearing loads both in the range of strength and in the range of steadiness are increased. The torsion moment and the lateral moment in the jib are reduced, the cross-section becomes

slimmer, the shell radii are narrower and the stability of the shells is increased.

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